







#### Leveling Included 670 New and 35 Existing Benchmarks (see kmz File)







# Benchmark Routes, Photos, KMZ's & Descriptions available on CCSF Website





# Detailed BM Descriptions available in a Spreadsheet on the CCSF Website

	10	12° DOMED STREE ANCHER PR	SCONNEST CONER OF SEACH & PONELL	In province agreement of the second works, the resonance of the province of the second of the secon	104200	fical	£(+).422m	Denselat, escaled	LOOPA
919623	MEY .	12° DOMEDI BITELL ANCHOR PRI	SOUTHING OF CORRESS OF BEACH &	IN SERVICE, IN DOCTIONS ST. INJOINT VERICA CENTER PACE OF CORE INTO THE ST. INJOINT AND ST. INFORMATION INTO THE ST. INTO THE ST. INTO THE ST. INTO	1043613	Nezri	B.+3405m	2009/14/14/2013	LOOP A
W18823	M.	12° EGNESI BTED ANCHER PR	SOUTHINGST COMES OF REACH &	SHE BRACE IF AT TRUCKNERMALLY OF FACE OF CURE & CATOR MARKS IF TRUCKNERMAT OF THERE USED & TANLOR IF TRUCKNERMAT OF THERE USED & TANLOR TO RESIDENCE OF CONTROL OF MARKS IF TRUCKNERMAT OF CHARKE LIGHT & BEACH IF TO RESIDENCE TO THERE LIGHT & BEACH IF TO RESIDENCE THERE LIGHT & BEACH IF TO RESIDENCE THERE LIGHT & BEACH IF TO RESIDENCE THERE LIGHT & BEACH IF	11343012	No.22	E + 31656	SIBLACS, SASHES	LOOPA
#19624	521	IF DOMES	SOUTHWEST COANER OF BEACH &	NUMERIA DALANENS & SIS BEACH ST	11040892	10123	EL + 4.23509	UNHALSY, 142615	LOOPA

# Specification and Procedures Second Order Class I

- The "Federal Geodetic Control Subcommittee (FGCS) Specifications and Procedures to Incorporate Electronic Digital/Bar-Code Leveling" (ver. 4.1) for Geodetic Leveling -
- Combined with best practices, experience and "Murphy" in a document titled "2013 Second Order Leveling Network Specification and Procedures"

#### **DATA COLLECTION & EQUIPMENT**

- Field Surveys: Three person crew committed about 1/3 time from January-October 2013
- Instrument: Leica DNA10 electronic digital level and a pair of 4.05 meter Leica GKNL4 fiberglass bar code rods
- The DNA10 level was calibrated by Leica prior to the survey and a level collimation test (peg test) was performed prior to each field day of operation







#### Leveling Demonstration & Validation Survey

Required all personnel to *demonstrate* their proficiency in the instrument operation, their understanding of the "Leveling Specification & Procedures" and that the equipment was operating correctly



	Length	Closure	1stOrd/I	2ndOrd/I		Length	Closure	1stOrd/I	2ndOrd/I
Loop	Km	mm	mm= 3√km	mm= 6√km	Loop	Km	mm	mm= 3√km	mm= 6√km
A	24.3	0	15	30	L	1.1	1	3	6
В	25.7	9	15	30	М	0.6	1	2	5
С	11.4	-3	10	20	N	0.5	2	2	4
D	10.1	-4	10	19	0	0.5	2	2	4
Е	5.8	-3	7	14	Р	0.8	0	3	5
F	6.8	1	8	16	Q	0.8	0	3	5
G	3.1	1	5	10	R	2.4	0	5	9
H	2.6	1	5	10	S	3.5	-16	6	11
I	1.8	-1	4	8	т	2.4	0	5	9
J	1.6	1	4	8	σ	3.5	1	6	11
	0.6		2	5	V	4.8	9		13

Level Network & High Precision Network 22 Loops – 115 km included the High Precision Network



#### FINAL NETWORK ADJUSTMENT

- All loops were combined in a Minimally Constrained Adjustment fixing one BM to develop final heights
- Adjustment Residuals less than +/-1 mm
- The combined network adjustment statistically resulted in 2mm\*√km (First Order Class I = 3mm\*√km)

#### NAVD88 DATUM RECOVERY:

- NAVD88 is <u>realized</u> by NGS benchmarks leveled circa 1977 and 1989 and published in the original 1991 national adjustment
- As a result of the 2013 leveling, the realization of NAVD88 in San Francisco is based on an extensive recovery of "First Order" NGS benchmarks in the City.



#### Datum Recovery:

Criteria for Benchmarks deemed the best candidates for recovering the NAVD88 Datum

- Height derived from the 1991 national adjustment of NAVD88
- Accuracy classification of "First Order"
- Stability Classification of A or B (on a scale of A-D)
- All such candidates were searched for and 14 recovered in the County



NAVD88 DATUM RECOVERY: Selecting a reference point for the adjustment that best fit all the candidate BM's

 The record height at NGS Benchmark HT2255 located east of the Golden Gate Bridge was found to agree with a best fit of all candidate Benchmarks.

#### NAVD88 DATUM RECOVERY: Selecting a reference point that best fits all the candidate BM's

- HT2255 has the following attributes:
- First Order Class I classified as a stability "A" benchmark set in a bedrock formation and expected to remain stable,
- Agreed 1-2 mm with two nearby stability "B" benchmarks (HT0698 and HT0700) a further indication of long term stability,

Analysis of				Record	Record t	to Computed	l Height
Analysis of	Name	NGS PID	Status-Stability	NAVD88 Ht	All BM's	All Adj'd	AB Adj'd
NOO	BM990515	HT0515	VertCon	91.520	0.007	-	
NGS	BM990516	HT0516	VertCon	92.710	0.013		
	BM990517	HT0517	VertCon	90.070	0.008		
Ronchmarke	BM990604	HT0604	VertCon	4.690	0.001		
Deneminarks	BM990687	HT0687	Adjusted-CD	3.779	0.001	0.001	
	BM990692 *	HT0692	Adjusted-AB	4.754	-0.021	-0.021	
	BM990697	HT0697	Adjusted-CD	5.029	-0.006	-0.006	
	BM990698	HT0698	Adjusted-AB	4.249	-0.001	-0.001	-0.001
	BM990700	HT0700	Adjusted-AB	4.237	-0.002	-0.002	-0.002
	BM990701=111	HT0701	Adjusted-AB	4.008	-0.008	-0.008	-0.008
	BM990702	HT0702	Adjusted-AB	3.996	-0.012	-0.012	-0.012
FIXEd H12255:	BM990705	HT0705	Adjusted-CD	4.833	-0.002	-0.002	
	BM990713 *	HT0713	Adjusted-AB	3.409	-0.045		
The differences	BM990720	HT0720	Adjusted-AB	3.800	0.014	0.014	0.014
	BM990721	HT0721	Adjusted-CD	3.563	-0.007	-0.007	0.005
from record	BM990724	HT0724	Adjusted-AB	6.221	0.005	0.005	0.005
nomrooora	BM990728	HT0728	Adjusted-AB	4 385	-0.009	-0.004	-0.004
heights to	BM990759	HT0759	Adjusted-CD	3.505	-0.010	-0.010	0.005
neights to	BM990781	ur0781	VertCon	7 150	0.008	0.010	
adjusted beights	BM991843=104	HT1843	VertCon	7.560	-0.010		
aujusteu neigints	BM992254	HT2254	VertCon	4.370	-0.003		
in motors aro	BM992255	HT2255	Adjusted-AB	5.844	0.000	0.000	0.000
in meters are	BM992259	HT2259	Adjusted-CD	51.430	-0.003	-0.003	
listed in the right	BM992261	HT2261	Adjusted-AB	46.912	0.013	0.013	0.013
instea in the right	BM992262	HT2262	Adjusted-CD	52.738	0.008	0.008	
41	BM992263	HT2263	Adjusted-CD	69.619	0.014	0.014	
three columns	BM992267	HT2267	Adjusted-CD	67.480	0.012	0.012	
	BM992268	HT2268	Adjusted-CD	102.431	0.021	0.021	
	BM992273	HT2273	Adjusted-CD	58.189	0.009	0.009	
	BM993538	HT3538	Adjusted-CD	3.734	-0.023	-0.023	
	BM993541	HT3541	Adjusted-AB	5.601	0.004	0.004	0.004
	BM995209=201	AE5209	Adjusted-AB	3.669	-0.010	-0.010	-0.010
	BM997677=202	AB7677	3rd Order	23.690	0.071		
	вм997679=107	AB7679	GPS Observation	3.700	-0.003		
				Number =	35	25	12
				Mean =	0.001	0.000	U.000
	<pre>* = outlier</pre>	1	1	Std.Dev.=	0.017	0.011	U.008

#### HISTORICAL CCSF LEVELING FOUND CONSISTENT WITH THIS SURVEY

- CCSF conducted extensive precise leveling surveys between 1999-2002 using a first order NA3003 Digital Level and invar rod with struts
- 37 BM's were recovered. The average difference from the 2002 Record Ht's to this survey is +1 mm with a Std. Dev. of 9 mm.

2013	2002	Survey	2002-2013	2013	2002	Survey	2002-2013
Name	Name	Ht(m)	Difference	Name	Name	Ht(m)	Difference
BM10249	т-0089	3.479	0.005	BM10299	BM-0005	3.471	-0.006
BM10251	<b>T-0087</b>	3.467	-0.007	BM10300	T-0179	3.565	-0.005
BM10252	T-0086	3.485	-0.014	BM10303	BM-0004	3.441	0.000
BM10254	T-0085	3.369	-0.007	BM10310	<b>T-0181</b>	3.469	-0.006
BM10255	<b>T-0017</b>	4.721	0.000	BM10427	<b>T-0169</b>	56.460	0.016
BM10256	T-0016	4.716	-0.001	BM10450	<b>T-0144</b>	11.401	0.004
BM10258	т-0083	4.506	-0.013	BM10468	<b>T-0121</b>	8.516	0.044
BM10261	т-0080	4.392	-0.017	BM10469	т-0120	7.066	-0.004
BM10263	т-0078	5.323	-0.014	BM10522	т-0109	22.196	0.001
BM10264	т-0077	5.509	-0.016	BM990604	HT0604	4.691	0.000
BM10265	<b>T-0076</b>	5.677	-0.012	BM990726	HT0726	6.990	0.004
BM10271	т-0069	12.953	0.005	BM990728	HT0728	4.378	-0.002
BM10272	т-0068	13.305	0.003	вм990781	HT0781	7.158	0.000

0.003 BM992267 HT2267

-0.005 BM992268 HT2268

0.028 BM993541 HT3541

-0.001 BM997677 AB7677

0.001

-0.004 BM99999 SM No.1

67.480

5.601

23.757

59.213

102.431

0.012

0.021

0.004

0.004

0.010

#### SAN FRANCISCO VERTICAL DATUMS

- The new "SFVD13" realization of the NAVD88 Datum supersedes previous NGS Benchmark Heights, and the old "SF Datum"
- The City and County Surveyor has determined that the conversion from the CCSF 2013 NAVD88 Datum to the <u>old</u> City Datum, henceforth shall be the following:
  - Conversion Constant (Feet)
  - 2013 NAVD88 Datum 11.35 feet = City Datum

BM10273

BM10276

BM10278

BM10293

BM10294

ВМ10295 Т-0161

т-0067 13.010

8.136

5.853

4.715

4.266

6.590

T-0065

T-0064

**T-0176** 

T-0177

#### **GPS SURVEYS**

- In July 2013 a high precision GNSS survey observed all CCSF-HPN points (101-120)
- The ellipsoid heights were combined with a refined Geoid 2012A Model to compute NAVD88 Heights and found to agree with the leveling survey, averaging 4 mm (0.01') and a range of +/- 7mm (0.02')
- CCSF intends to utilize GNSS and a local RTN to replace conventional differential leveling for determining heights in the future at the subcentimeter level

#### ACCURACY

- Relative accuracy of adjacent monuments is expected to be less than 0.001 meters (0.003')
- 95% Error of the heights range 1 to 12 mm relative to fixed constraint HT2255 (average 9 mm)
- Absolute accuracy of the heights is dependent on the recovery of the NAVD88 Datum which was based on a best fit of 12 BM's with a Std. Dev. of 8 mm

#### ACCURACY

- This survey is classified as Second Order Class I;
- however, the average actual loop closures of 3 mm (0.01 feet),
- the agreement with 2002 precise leveling
- and the results of the GNSS survey indicate results consistent with First Order specifications were obtained.

# 2014 Densification (112 km) of the Leveling Network (227 km total)



#### **Report Contents**

**OVERVIEW** 

**DATUMS, REFERENCE SYSTEMS & HISTORY** 

VERTICAL NETWORK

EQUIPMENT, DATA COLLECTION

**ADJUSTMENTS** 

NAVD88 DATUM RECOVERY

HISTORICAL LEVELING & SAN FRANCISCO CITY DATUM



# Leveling Survey Report

of the CCSF 2013 Second Order Leveling Survey (pdf) Available At http://www.sfdpw.org/index.aspx?page=1781 (Google "HPN Survey")

**Report Attachments** 

- NAVD88 (2013) Orthometric Height List
- Benchmark Descriptions, Photos & KMZ Files
- "CCSF 2013 2<sup>nd</sup> Order Leveling Network Specification and Procedures"

5/1/2014





#### **PROJECT OVERVIEW**

- The Survey established 20 high precision control points in July 2013 utilizing GNSS technology
- The Network is referred to as the "<u>City & County of San</u> <u>Francisco High Precision Network</u>" (CCSF-HPN)
- Purpose: Provide a framework for densification, support the City's GIS, and provide a Deformation Network to measure secular and episodic ground movements
- Under the old classification system, the network is classified as a "B" Order Survey 1:1,000,000





# Planning/Preparation

HPN-101 North Central Radial Base



# Planning/Preparation



#### Station Recovery & Obstruction Diagram, Photos and KMZ Files are available on the Website





#### **EQUIPMENT CALIBRATION**

• Fixed Height Poles calibrated for height and plumb



#### **CREW CALIBRATION**

 Validation Survey: Verify the crews understand their assignments, procedures, receiver operation, filling out the paperwork, communication protocols and verify the equipment was operating properly before starting the field campaign.



#### **OBSERVATIOIN & DATA COLLECTION**

#### GNSS Survey:

- Constellation: 32 US Navstar GPS satellites and 24 Russian GLONASS satellites
- Satellite Observed: 12-21 satellites observed with a minimum of 6 GPS and 6 GLONASS; GDOP< 2;</li>
- Elevation Mask set at 10° and post-processed at 15°
- Observables: GPS L1 & L2, GLONASS L1 & L2

#### **OBSERVATIOIN & DATA COLLECTION**

- GNSS Survey:
- Space Weather: Planetary K Index = 1-3 (gauges ionospheric activity on a scale of 0-9, <5 preferred)</li>

Weather: Generally overcast marine layer and mild temperatures throughout the five day campaign

#### DATA PROCESS

- Absolute Antenna Models used in processing baselines; imported from the NGS and listed in the Survey Report
- Vectors (baselines) were processed in IGS08 (WGS84) with the Precise Ephemeris imported from the NGS (GPS) and IGS (GLONASS)
- Post-Processing: Leica Geomatics Office (LGO) v8.1
- Network Adjustments: Starnet v7.2.

#### **REGIONAL NETWORK**

Four nearest NGS CORS stations (TIBB, P224, WINT & P176) were included and are the basis for recovering the IGS08(2005) and NAD83(2011) Datums

Four CGPS stations (EBMD, P178, UCSF and MHDL) were included to add strength and redundancy to the Network.



# <image>

#### **REGIONAL NETWORK STATISTICS**

The network contained 57 vectors averaging 20 km (12 mi.) in length, max. 38 km

Each vector represents three 24 hour observations staggered every other day

Min. Constrained Adjustment 2D Residuals Av. 2 mm, Std. Dev. 2 mm, Max. 10 mm; Vertical Residuals Av. 2 mm, Std. Dev. 2 mm, Range -7 to +8 mm



#### HIGH PRECISION NETWORK (HPN) SURVEY

Field campaign took 5 days during the week of July 15-19, 2013 (average epoch 2013.54)

Four crews operated Four Leica GS15 GNSS Receivers on FHP's

HPN points were occupied for 45 minutes at 15 sec. epoch rate



Field Campaign: Day-1 - Radial Network A Base Receiver occupied #101 while three crews occupied 19 remaining points at will











#### Session Occupations & Processing Non-Trivial Lines



# <text>

Survey

#### **HPN STATISTICS**

The network contained 83 non-trivial vectors averaging 4 km (2 1/2 mi.) in length, maximum 8 km

Min. Constrained Adj. Vector Residuals: 2D Av. 3 mm, Std. Dev. 2 mm, Max. 10 mm; Vertical Av. 3 mm, Std. Dev. 3 mm, Range -9 to +16 mm





Google earth



#### **DATUMS - REFERENCE SYSTEMS**

- Geometric Datums (3D) and Reference Frame
- NAD83 (2011) Epoch 2010.00 & Epoch 2013.54
- **IGS08 (2005) Epoch 2013.54 (July 17, 2013)**
- Reference Network
- NGS CORS (Continuously Operating Reference Stations)
- Vertical Datum
- CCSF NAVD88 2013 Vertical Datum (SFVD13)
- Reference Network
- Reference by the HPN

Stat	dN	dE	dZ	
 101	-0.000	-0.000	-0.000	
 102	-0.000	0.000	0.000	Coordinate Changes
 103	0.002	0.001	0.001	from Notwork to a Redial
 104	0.001	-0.001	-0.002	from Network to a Radial
105	-0.003	-0.001	0.002	or "Hub" Solution
106	-0.004	-0.000	0.000	(meters)
107	0.001	0.001	0.003	(
108	0.004	-0.002	0.001	
109	-0.003	-0.001	0.003	
110	-0.001	-0.000	0.003	
111	-0.002	0.001	-0.002	
112	0.001	-0.002	-0.001	
113	0.002	0.000	-0.001	
114	0.001	0.001	-0.001	
115	0.002	-0.000	-0.001	
116	-0.000	0.002	0.002	
117	0.000	-0.000	-0.002	
118	0.001	0.002	-0.002	
119	-0.002	-0.000	0.004	79
120	-0.000	-0.001	-0.005	

#### **DATUM RECOVERY**

Four nearest <u>operating</u> CORS were the basis for recovery of the IGS08 & NAD83 Datums

- IGS08 and NAD83 positions and velocities were obtained from the NGS CORS website
- HTDP model v3.2.3 was used to move positions between epochs for CORS operating <2.5 years</li>
- Six network adjustments were processed to develop geodetic and plane coordinates in two reference frames at two different epochs

# HTDP = Horizontal Time Dependant Program

- Why HTDP? Why Change Epochs?
- SF Bay Area is crossed with multiple faults and the CORS are each moving in a different direction and speeds.
- The CORS do not have the same relationship today as in 2010.00; therefore, must process in real time by moving the 2010.00 positions to 2013.54 (date of field survey).

#### REGIONAL NETWORK

Four NGS CORS: TIBB P224 WINT P176 Four CGPS stations: EBMD P178 UCSF MHDL CCSF (Private RTN Sta.)



#### **OVERVIEW of the ADJUSTMENTS**

- #1 MA and #2 CA: Developed positions in <u>IGS08(2005) 2013.54 Epoch</u> for referencing future secular and episodic movements
- #3 MC and #4 CA: Developed positions in <u>NAD83(2011) 2013.54 Epoch</u> on the Regional Network for the purpose of establishing NAD83(2011) in the City
- #5: Developed positions in <u>NAD83(2011) 2010.00</u>
  <u>Epoch</u> for the HPN in the City
- #6: Analyzed the Geoid 2012A Model for accuracy and consistency with the 2013 Leveling Network

#### System Test: Compute a 3D 7-Parameter Transformation of the Measured Network to Best Fit the IGS08 Positions of the CORS Stations

- Verify the consistency of the network computed with the precise ephemeris and the NGS IGS08 positions of the CORS Stations. The expectation is no change.
   Datum Transformation
  - Scale Factor = 1.000000685 (1:15m)
- Rotation Around North Axis = -0.07 Sec
- Rotation Around East Axis = -0.06 Sec
- Rotation Around Vert. Axis = -0.01 Sec

•	Station	dN	dE	dZ
•	P176	0.003	-0.001	0.002
•	P224	0.006	0.002	0.006
-	TIBB	-0.005	-0.001	-0.003
	WINT	-0.004	0.000	-0.005

#### IGS08(2005) Epoch 2013.54 Adjustment #1

Steps:

- 1- IGS08(2005) positions of the CORS obtained from NGS
- 2- IGS08(2005) positions moved to 2013.54 with HTDP
- 3- WINT was fixed in a Minimally Constrained Adjustment (includes four CORS, four CGPS stations, RTN CCSF and the HPN
- 4- Coordinate differences (closures) reviewed at other three CORS

#### 5/1/201

#### IGS08(2005) Epoch 2013.54 Adjustment 1: 3D Minimally Constrained

#### Coordinate Differences: IGS08 to Computed

•	Station	dN (m)	dE (m)	dZ (m)_	
•	P176	0.007	-0.004	0.006	
•	P224	0.012	0.003	0.002	
•	TIBB	0.003	-0.001	-0.015	
•	WINT	0.000	0.000	0.000	FIXED
•	Diff. N 3 to	12 mm,	E -4 to 3 mm,	Up -15 to 6	6 mm

#### IGS08(2005) Epoch 2013.54 Adjustment 2: 3D Constrained Adjustment

- All four CORS were constrained to develop IGS08(2005) 2013.54 Epoch positions on the CGPS and the HPN Stations
- UCSF position obtained from OPUS used as a check (mean of three 24 hours observations)
- Coordinate Difference: UCSF/OPUS to Computed (m)
- Station dN dE dZ
- UCSF -0.001 0.001 -0.014 CA/free
- Difference of 1mm at UCSF indicates the compatibility with the NGS process

#### NAD83(2011) Epoch 2013.54 Adjustment #3

#### Steps:

- 1- NAD83(2011) 2010.00 Epoch positions of the CORS obtained from NGS Data Sheets
- 2- NAD83(2011) 2010.00 Epoch positions moved to 2013.54 with HTDP
- 3- WINT was fixed in a Minimally Constrained Adjustment (includes four CORS, four CGPS stations, and CCSF)
- 4- Coordinate differences (closures) reviewed at other three CORS

NAD83(	2011)	Epoch 2	013.54
Adjustment 3	: 3D N	linimally	Constrained

Coordinate	Differenc	es: NAD83	8(2011) to C	on
Station	dN	dE	dz	
P176	0.006	-0.004	0.005	
P224	0.012	0.004	0.006	
TIBB	0.004	-0.001	-0.010	
WINT	0.000	0.000	0.000	F
Aax. Closures	N 12mm,	E 4mm,	Up 10mm	

#### NAD83(2011) Epoch 2013.54 Adjustment 4: 3D Constrained

- All 4 CORS were constrained to develop NAD83(2011) 2013.54 Epoch positions on the CGPS
- A 2013.54 position of UCSF (in SF) was obtained from SOPAC/SECTOR as a check.
- Coord. Differences: From UCSF to Computed
- Station dN dE dZ
- UCSF 0.004 -0.001 -0.004 CA/free

Note, SECTOR is referenced to NAD83(2007), whereas this adjustment is referenced to NAD83(2011)

#### NAD83(2011) Epoch 2010.00 Adjustment #5 (getting back to 2010)

#### Steps:

- 1- NAD83(2011) 2013.54 Epoch positions of UCSF, MHDL & CCSF were obtained from Adjustment #4
- 2- NAD83(2011) 2013.54 Epoch positions moved to the NAD83(2011) 2010.00 Epoch with HTDP
- 3- UCSF fixed in a Minimally Constrained Adjustment (included the HPN, MHDL & CCSF)
- 4- Coordinate differences (closures) reviewed

		NAD83(	2011) E	poch 2	010.	00	
	Adiu	stment {	5: 3D Mi	nimally (	Const	traine	ed
•	Coordi	nate Diffe	rences: N	AD83(201	1) to C	Compi	ited
	Stat.	dN (m)	dE	dZ_	Ep	och	
	UCSF	-0.000	-0.000	-0.000	201	0.00	FIXD
	MHDL	-0.003	0.003	-0.006	201	0.00	
	CCSF	-0.005	0.002	0.007	201	0.00	
•	A 2010 from O observ	.00 Epoch PUS as a ations.	position check bas	of UCSF v se on thre	vas ok e 24 h	otaine our	d
	Coord.	Differenc	es: From	UCSF/OP	JS to	Comp	uted
	Statio	on dN	ć	iE	dZ		
	UCSF	-0.00	4 0.0	001 -0	.013	CA/f1	ree

#### NAD83(2011) Epoch 2010.00

**Coordinate Differences from HTDP to Computed** 

- The closures on the HTDP positions of MHDL and CCSF are less than the noise level of the HTDP model.
- Therefore, the results of this adjustment were held to established NAD83(2011) 2010.00 Epoch positions on MHDL, CCSF and the City's HPN.

#### NAD83(2011) Epoch 2010.00 Adjustment 5: HPGN in the City

 Coordinate Differences at the HPGN stations: NGS NAD83(2011) 2010.00 Epoch to Computed

Stat. dN	(m) dE	dZ (EH)	Epoch	Source
<b>■ 107 -0</b> .	034 0.007	-0.040	2010.00	NGS Candlstck
■ 201 -O.	029 0.002	-0.045	2010.00	NGS Tidal
■ 202 -0.	053 0.017	-0.031	2010.00	NGS Sloat

#### Adjustment 6: Geoid Model Analysis

- Two Methods for incorporating Ellipsoid Heights and Geoid Heights to Determine NAVD88 Orthometric Heights are discussed here.
- Method One: <u>Approximates</u> NAVD88 Heights by applying the hybrid Geoid 2012A heights to the measured NAD83 Ellipsoid Heights using the equation H=h-N
- (H= Orthometric Ht, h=Ellipsoid Ht, N=Geoid Ht).
- The accuracy of this method in San Francisco is about 0.06 meters (Note, Geoid 12A is a <u>hybrid</u> model, compatible with NAD83(2011) Ellipsoid Hts)

#### Geoid Model Analysis Adjustment #6

- Method Two: Takes advantage of the <u>relative</u> precision of geoid heights. The Geoid 2012A Model was incorporated in a seven parameter transformation to best fit the <u>leveled</u> NAVD88 2013 Heights on the 20 HPN points
- Transformation Explained:
- Two horizontal constraints, scale fixed to 1.0 and heights loosely weighted
- Least Squares solution allows the geoid to float and rotate around the north and east axis to best fit the vertical constraints.

#### Geoid Model Analysis Adjustment #6

- Method Two: Takes advantage of the <u>relative</u> precision of the geoid model heights.
- The Geoid 2012A Model was incorporated in a seven parameter transformation to best fit the <u>leveled</u> NAVD88 2013 Heights on the 20 HPN points
- Least Squares solution allows the geoid to float and rotate around the north and east axis to best fit the vertical constraints.
- The rotations represent the tilts applied to the Geoid 2012A surface model to best fit the leveled NAVD88 2013 Heights

#### Geoid Model Analysis Adjustment #6

 The rotations represent the tilts applied to the Geoid 2012A surface model to best fit the leveled NAVD88 2013 Heights

Column "A" are Differences from Leveled Ht to Modeled Column 'A': Mean = zero, Range = -7 to +7 mm, Std Dev = 4mm, Solved rotations = +0.21" around the N and +0.24" around the E axis

	А	в	C	D=C-B	F	E=E-D
Point	Diff's	NAVD88 Hts	NAD83 EH	Meas'd GH	2012A GH	Diff.
101	-0.003	150.799	118.188	-32.611	-32.548	0.063
102	0.004	170.991	138.344	-32.647	-32.587	0.060
103	0.004	46.352	13.592	-32.760	-32.712	0.048
104	0.000	7.550	-25.278	-32.828	-32.771	0.057
105	-0.004	56.489	23.607	-32.882	-32.817	0.065
106	-0.007	110.302	77.575	-32.727	-32.653	0.074
107	0.006	3.698	-28.944	-32.642	-32.574	0.068
108	0.000	4.484	-28.109	-32.593	-32.523	0.070
109	-0.004	3.461	-29.098	-32.559	-32.491	0.068
110	0.003	3.279	-29.261	-32.540	-32.486	0.054
111	0.003	4.000	-28.605	-32.605	-32.555	0.050
112	-0.004	54.344	21.692	-32.652	-32.593	0.059
113	-0.001	74.816	42.159	-32.657	-32.598	0.059
114	-0.001	99.656	66.915	-32.741	-32.681	0.060
115	0.003	61.448	28.692	-32.756	-32.697	0.059
116	0.007	89.985	57.292	-32.693	-32.635	0.058
117	-0.004	117.172	84.526	-32.646	-32.572	0.074
118	0.003	78.553	45.947	-32.606	-32.543	0.063
119	-0.003	18.941	-13.634	-32.575	-32.511	0.064
120	-0.002	85.887	53.304	-32.583	-32.524	0.059
Mean=	0.000	63.188	30.513	-32.675	-32.613	0.062

# Leveled Hts & GNSS Modeled Hts at HPN 101 & 102 Agree 6 mm (0.02')



#### **Determine Orthometric Hts**

The accuracy will be the combined accuracy of the NAVD88 height of the HPN points, the accuracy of the measured ellipsoid height differences, the relative accuracy of the geoid heights and the residual tilt between the geoid modeled surface and the actual geoid surface. The effect of the tilt listed above (rotations of +0.213 and +0.243 seconds around the north and east axis) is 1.6 mm per kilometer (0.008' per mile) or less and would be absorbed in a constrained adjustment. The largest source of error is usually in the measured ellipsoid heights.

#### **Determine Orthometric Hts**

- Following the specifications and procedures used in this survey, an orthometric height accuracy of 0.007 meters (0.02 feet) was achieved at the HPN Stations utilizing GNSS.
- CCSF is in the process of developing procedures to utilize the local RTN Network to establish centimeter level orthometric heights.

#### **NGS Gravimetric Geoid Model**

- USGG2012 Model used in a trial transformation to best fit the NAVD88 heights of the HPN points
- Returned results similar to the hybrid model; however, the rotations were +0.138 and +0.120 seconds around the north and east axis (negligible improvement as expected)

#### Accuracy

Vector Residuals: Resulting from the minimally constrained adjustment in meters. Two Dimensional Residuals Vertical Residuals (absolute values) No. Average Std.Dev. Max. Average Std.Dev. Range CCSE HPN 83 0.003 0.002 0.010 -0.009 to +0.016 0.003 0.003 Regional CORS 57 0.002 0.002 0.010 -0.007 to +0.008 0.002 0.002 Local Accuracies: Resulting from the minimally constrained adjustment at the 95% Level of Confidence in meters Vector Lengths(m) Relative Dist. Error Rel.Vert. Error Network Vary Average Average Max. Precision Average Max. 0.003 0.004 CCSF HPN 1675-8291 4267 0.004 0.005 1:1,070,000

0.003 0.004

Regional 5322-37896 20224 0.003 0.003 1:6,740,000

# **Local Accuracy**

 Local Accuracies: Resulting from the minimally constrained adjustment at the 95% Level of Confidence in meters

	Relat	ive Dist	Rel.Vert. Error		
Network	Average	Max.	Precision	Average Max.	
CCSF HPN	0.004	0.005	1:1,070,000	0.003 0.004	
Regional	0.003	0.003	1:6,740,000	0.003 0.004	

#### **Computing Network Accuracy**

- RMS's for the Latitude, Longitude & Ellipsoid Heights of the CORS stations were obtained from the "Short Term Time Series" at the NGS CORS website,
- and used to in a <u>weighted</u> constrained adjustment to develop the Network Accuracies on each point (Public Resources Code requirement)

#### **Computing Network Accuracy**

- Standard Deviations for three of the four CORS were not available (less than 2.5 years of data),
- therefore the "Short Term Time Series" were used for all CORS for consistency

# NGS Reference Document



		N	etwo	rk Acc	curacy		
This table	allow	s use	ers to	calculat	the pr	opagated	d network
error fo	or fut	ure si	urveys	s based	on the	HPN pos	itions
			NETWO	RK ACCURACY i	n Meters		
		Coordi	nate Std.	Deviations	Network Accy.	95% Confidence	
	Station	Latitude	Longitude	Ellipsoid Ht	Horizontal	Ellipsoid Ht	
	101	0.002	0.002	0.004	0.005	0.008	
	102	0.002	0.002	0.004	0.005	0.008	
	103	0.003	0.003	0.004	0.006	0.009	
	104	0.003	0.003	0.004	0.006	0.009	
	105	0.002	0.002	0.004	0.006	0.009	
	106	0.003	0.003	0.004	0.006	0.009	
	107	0.003	0.003	0.004	0.006	0.009	
	108	0.002	0.002	0.004	0.006	0.009	
	109	0.003	0.002	0.004	0.006	0.009	
	110	0.002	0.002	0.004	0.006	0.008	
	111	0.002	0.002	0.004	0.006	0.008	
	112	0.002	0.002	0.004	0.006	0.008	
	113	0.002	0.002	0.004	0.006	0.008	
	114	0.003	0.002	0.004	0.006	0.009	
	115	0.002	0.002	0.004	0.006	0.008	
	116	0.003	0.002	0.004	0.006	0.009	
	117	0.002	0.002	0.004	0.006	0.009	
	118	0.002	0.002	0.004	0.006	0.008	
	119	0.002	0.002	0.004	0.006	0.008	
	120	0.002	0.002	0.004	0.006	0.008	
	CCSF	0.002	0.002	0.004	0.005	0.008	
	EBMD	0.002	0.002	0.004	0.004	0.008	
CODEN	MHDL	0.002	0.002	0.004	0.004	0.008	
CORS 2	P176	0.001	0.001	0.004	0.004	0.008	
P176	P178	0.002	0.002	0.004	0.004	0.008	
P224	P224	0.001	0.001	0.004	0.003	0.008	
TIBB	TIBB	0.001	0.001	0.004	0.004	0.008	
WINT	UCSF	0.001	0.001	0.004	0.003	0.008	
VVIINT	WINT	0.001	0.001	0.004	0.003	0.008	

#### Transformation: 1999 NAD83 (1991.35 Epoch) SPC > 2013 NAD83 (2011) 2010.00 Epoch SPC

		INPUT COORDINA	ATES (Feet)		
1999	NAD83(1991) 199	1.35 SPC	201	.3 NAD83 (2011	)2010.00 SP
PT#	North(1)	East(1)	PT#	North(2)	East(2)
CANDLEST	ICK 2085128.546	6013911.480	107	2085130.260	6013910.28
TIDAL	2121772.462	5993470.060	201	2121774.233	5993468.88
SLOAT	2095678.561	5984226.406	202	2095680.395	5984225.1
ARMY	2100667.364	6012652.104	203	2100669.127	6012650.9
	TRANSFO	RMATION SOLUT	ION RESIDUA	LS (Feet)	
1999	2013	North	East	N.Azim & Dis	t
CAND	LESTICK 107	-0.019	+0.018	138° 0.026	
TIDA	L 201	-0.031	-0.009	197° 0.032	
SLOA	т 202	+0.034	-0.011	342° 0.036	
ARMY	203	+0.015	+0.003	11° 0.016	
Root Mea	n Square of the	North and East	st Residual	.s = 0.02	
Scale Fa	ctor = 1.00000	077 Stand	dard Deviat	ion = 0.000	00078
Rotation	= +0° 00'	00.4" Stand	dard Deviat	$ion = 0^{\circ} 00$	00.2"
TRANSFOR	MATION EQUATION	S: N2=A1*N1.	-A2*E1+A4	E2=A2*N1+A1	*E1+A3
	00007745 30- 0	0000019602	3= -9 9625	1 24-11 90	684
A1= 1.00	00007745 MZ= 0	.0000019002 1		<u>, uz- 11.)</u>	003

#### Accuracy Classification per FGDC-Std-007, 2-1998

- Following the FGDC "Geospatial Positioning Accuracy Standard, Part 2, Geodetic Control Networks" (FGDC-Std-007, 2-1998), at the 95% Level of Confidence this survey is classified as.....
- Local Horizontal Accuracy Classification is 5 mm
- Local Ellipsoid Height Acc. Classification is 5 mm
- <u>Network</u> Horizontal Accuracy Classification is 1 cm
- Network Ellipsoid Height Acc. Classification is 1 cm
- This Survey conforms to the requirements of Public Resources Code Section 8801 through 8819 and 8850 through 8880.

#### New CCSF Coordinate System

City & County of San Francisco Coordinate System 2013 (CCSF-CS13)

 CCSF-CS13: A low distortion grid projection designed for and centered on the County

Minimizes grid-ground differences in distances

- CCSF-CS13 provides a grid scale distortion of less than 1:100,000 (10 ppm) in most parts of CCSF
- For the average combined factors of the 20 HPN points, a ground distance of 1000 foot equals
- 1000.003 feet in the CCSF-CS13 and
- 999.925 feet in SPC Zone 3

#### City & County of San Francisco Low Distortion Projection

- Projection surface was positioned at the most common ground height so that the combined scale factor is 1.0 and the distortion is zero
- Projection Surface Height
- Ellipsoid Height = 44.50 meters (146.0 feet);
- NAVD88 Height = 77 meters (253 feet)
- (see Purple Contour on next Slide)
- Note, Changes in height increases/decreases the scale 4.8 ppm for every 30.5 meters (100 foot)

#### CCSF-CS13: PPM (Distortion) Contours Purple= 0, Yellow= -10, Green= +10 (Bill Hurdle)



#### City & County of San Francisco Low Distortion Projection

- CCSF-CS13 system is referenced to the GRS80 ellipsoid, centered in the NAD83(2011) 2010.00 Epoch reference frame (same as SPC)
- Therefore: Coordinates are referred to as NAD83 (2011) Epoch 2010.00 CCSF-CS13
- North coincides with NAD83 Geodetic North at the Central Meridian near the center of the City
- Convergence Angle varies +/- two minutes east-west across the City

#### City & County of San Francisco Low Distortion Projection

 <u>Projection specifications for input in user's software:</u> Projection: Transverse Mercator Ellipsoid: GRS-80 Scale: 1.000007 Latitude of Origin: 37°45'00" (37.75) Central Meridian: -122°27'00" (-122.45) False Northing: 24,000 meters (78,740 feet) False Easting: 48,000 meters (157,480 feet)

(same idea as SPC Projections only less local distortion)

#### **SUMMARY**

- CCSF sits between two major faults, the San Andreas & Hayward. Future re-surveys of the HPN will be conducted to determine secular and episodic movements in the City
- If future surveys of the HPN follow the specifications and procedures adopted for this survey, the relative accuracy of measured movements is expected to approach 5 mm at the 95% level of confidence
- Statistically, this means the probability at the 95% level of confidence is that movement (signal) has occurred if the movement between two epochs is greater than the relative error (noise)

#### **RECOMMENDATION - SUMMARY**

- The differences in successive coordinates on a point can be used to estimate ground movements but they do not provide statistical information about the relative accuracies of movements; therefore the signal cannot be distinguished from noise.
- Measurements of temporal movements must be based on a rigorous simultaneous least squares adjustment of multiple independent observations at two different epochs for each point to compute the relative accuracy and thus the actual movement



#### RECORD of SURVEY #8080 Posted on the CCSF Website







#### Survey Report

of the 2013 CCSF High Precision Network Survey(pdf)

#### Available At

http://www.sfdpw.org/index.aspx?page=1781

(Google "HPN Survey)

#### Attachments

Record of Survey HPN Point Description/Obstruction Diagrams HPN KMZ Files Transformation Spreadsheets



# Final Thoughts About GN

- "..... it is far more important to have a somewhat faulty measurement of the spot where the line truly exists than to have an extremely accurate measurement of the place where the line does not exist at all"
- By A.C. Mulford, from "Boundaries and Landmarks", 1912